

# Flood Risk Screening and Surface Water Management Plan

## Holmston Farm BESS

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### **Revision History**

Issue	Date	Name	Latest changes
01	22.02.22	Daniel Cole	First issue

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## 1 Overview

#### 1.1 Introduction

Holmston Farm is a proposed battery-based energy storage system located just east of the town of Ayr, South Ayrshire, Scotland.

This report sets out the flood risk screening and surface water management plan for the proposed Holmston Farm battery energy storage system, which will house battery enclosures along with associated infrastructure and electrical equipment.

The battery storage system comprises battery enclosures with associated power conversion systems, transformers, a switchhouse and grid compliance equipment. All electrical equipment will be set on concrete foundations.

Drawing 04874-RES-LAY-DR-PT-001 included in Appendix A shows the proposed project layout. The compound area within the fence measures 0.70 hectares, the total area enclosed by the red line boundary measures 2.19 hectares.

## 2 Relevant guidance and legislation requirements

All drainage relating to the proposed energy storage facility will be constructed using best practice and in conformance with the requirements of the relevant regulatory authorities. The key legislation and guidance that will be adhered to are as follows:

- The EU Water Framework Directive (2000/60/EC).
- Scottish Planning Policy.
- The Water Environment (Controlled Activities) (Scotland) Regulations 2011.
- SEPA Pollution Prevention Guidance Notes (PPGs).
- Engineering in the Water Environment, Good Practice Guide, Temporary Construction Methods, First Edition, March 2009.
- Sewers for Scotland 3rd Edition.
- South Ayrshire Council Sustainable Design Guide
- CD 15 Environmental Report of Strategic Environmental Assessment Appendix H Strategic Flood Risk Assessment
- The Sustainable Urban Drainage Scottish Working Party (SUDSWP) Water Assessment and Drainage Assessment Guide.
- The SuDS Manual 2015. CIRIA C753.
- Soakaway Design BRE Digest 365.
- British Geological Survey (BGS) mapping.

## 3 Existing Information

#### 3.1 Site Location

Site can be located by National Grid Reference (NGR) N:236316, E:621202. A location plan is included in Appendix A.

The site sits within the east of a field adjacent to Holmston Roundabout, which lies on the eastern edge of Ayr. The field is bound to the west and south by the A77 and A70 respectively. A garden centre sits adjacent to the south of the site, abutting the southeast corner of the field. To the east of the site lies a substation and associated access track. The River Ayr passes a short distance north of the site.

### 3.2 Existing Land Use and Topography

A walkover survey of the site has been undertaken, and a topographical survey of the site extents carried out to confirm the existing land use and topography. Land on the site is partially used to grow conifer trees commercially, other areas on the site remain roughland with no apparent use.

Levels on the site slope down from east to west at a typical gradient of approx. 1:20. The substation access track abutting to the east is elevated approx. 5m above the site. This level difference is accommodated by a bank against the field's eastern boundary, sloping at an average of approx. 1:2.5.

Several shallow open drainage channels run across the site, approx. 1m wide and 0.5m deep, converging to an open-top inspection chamber in the west of the site.

A copy of the site topography survey plan is included in Appendix D.

#### 3.3 Ground Conditions

BGS mapping indicates that the site is underlain with a bedrock of Coal Measures Formation, described as sandstone, siltstone and mudstone with common coal seams. Superficial deposits on site are shown to comprise till, described as a mixture of clay, sand and gravel.

A Coal Mining Risk Assessment undertaken found the site was unlikely to be impacted by shallow mine workings.

## 3.4 Existing Hydrology / Drainage

Understanding of the site's existing hydrology / drainage is based on observations made during site visits, review of topographical survey information, and discussions with the landowner.

Stormwater is currently intercepted by the on-site shallow open drainage channels and conveyed into the open-top inspection chamber located in the west of site. A 150mm dia outlet pipe then conveys flows northwest, running underneath the wider field with approx. 100 - 200mm of cover. The outlet pipe discharges into a ditch, approx. 1.5m wide and 1m deep, that abuts the outer edge of the wider field's north-western boundary. The ditch terminates a short distance before the wider field's northern corner; flows then continue northwards in a buried pipe, ultimately discharging into the River Ayr.

The River Ayr is classified by SEPA as a 'moderate' quality watercourse. Annual monitoring data shows good status on all parameters except for aquatic plant 'Phyto benthos', which has 'moderate' status.

The site is located within the Ayr groundwater catchment, which is classified by SEPA as 'Poor' quality.

## 4 Flood Risk Screening

#### 4.1 Overview

A review of flood risk from various sources has been undertaken, and concludes that the site is at no risk of flooding. The proposed development will not increase flood risk anywhere on or off site due to the proposed measures outlined in Sections 5 and 6 of this report.

#### 4.2 Fluvial Flood Risk

The SEPA fluvial flood risk map shows there is no specific fluvial flood risk on or near to the site. The nearest area of fluvial flood risk to the site is approximately 100m to north, local to the River Ayr.

OS contouring indicates the area of fluvial flood risk local to the River Ayr lies at least 5m below site. The site is therefore considered to be at no risk of flooding from fluvial sources.

Figure 1 below shows a map of fluvial flood risk produced by SEPA covering the vicinity of site, overlaid with the proposed development application boundary.



Figure 1 - Excerpt from SEPA fluvial flood risk map, with proposed site boundary overlaid.

#### 4.3 Coastal Flood Risk

The SEPA coastal flood risk map shows there is no coastal flood risk on or near to the site.

#### 4.4 Surface Water Flood Risk

The SEPA surface water flood risk map shows there is no specific surface water flood risk on the site. A strip of surface water flood risk is shown along the east of the garden centre, which sits adjacent to the south of site. The garden centre is situated at a lower level than the site. The site is therefore currently considered to be at no risk of surface water flooding.

Figure 2 below shows a map of surface water flood risk produced by SEPA covering the vicinity of site, overlaid with the proposed development application boundary.



Figure 2 - Excerpt from SEPA surface water flood risk map, with proposed site boundary overlaid.

## 4.5 Flooding from Sewers

Scottish Water asset location plans show no sewers to exist within the vicinity of site. There is therefore considered to be no specific flood risk resulting from sewers.

## 4.6 Flooding as a Result of the Development

Whilst the proposed development will increase the total impermeable area on site, the measures set out in Sections 5 and 6 of this report will ensure there would be no increase in flood risk as a result of this development.

## 5 Drainage Design

### 5.1 Site Preparation

Topsoil on the site will be scraped off and set aside. The existing shallow open drainage channels on the site will be filled in with unbound granular material.

Proposed hardstanding areas and tracks will be graded with a minimum 300mm layer of unbound granular material. Depending on earthing requirements at detail design stage, the compound area may require a surface course of asphalt. To be conservative, an asphalt surface is assumed for the purposes of all calculations in this report.

The finished ground level of the proposed facility will be approximately 28.3m AOD. Finished levels across the compound will slope down to the west, in keeping with existing topography, at a gradient of approx. 1:50.

### 5.2 SuDS Hierarchy

In line with Scottish planning policy, a drainage solution for this proposed development shall be selected based on the principles of the SuDS Hierarchy as disclosed in the CIRIA C753 'The SuDS Manual'.

#### 5.2.1 Rainwater Harvesting

Rainwater harvesting is not applicable to this project; there are no facilities within the proposed development that have a demand for water.

#### 5.2.2 Infiltration

Prior to the detailed design of a drainage solution for the proposed development, infiltration testing will be undertaken on the site, performed to BRE 365 Digest.

It is anticipated that the ground underlying the site will not support an infiltration drainage solution, due to the following:

- Existing site drainage, as described in Section 3.4, demonstrates that surface water is not currently infiltrated into the ground, and must be conveyed off the site via constructed drains.
- BGS ground data indicates the site is underlain by superficial deposits of predominantly clay.

A drainage solution for the site is proposed in this report on the conservative assumption that an infiltration solution is not possible.

#### 5.2.3 Attenuate Rainwater in Ponds for Gradual Release

If infiltration to ground proves to be unfeasible, the next preference in the drainage hierarchy is to attenuate flows in a detention basin with a restricted discharge.

### 5.3 Proposed Surface Water Drainage Solution

The drainage strategy and indicative details of the proposed drainage infrastructure are included in Appendix B.

The drainage strategy proposed for the site will aim to maintain the existing hydrological pathway outlined in Section 3.4.

In the proposed drainage solution, all stormwater falling into the compound will run overground to the west and be intercepted by a filter drain along the compound's western boundary. From the filter drain, water will be conveyed to an attenuation basin situated adjacent to the west of the site. Water will then discharge from the basin into the ditch abutting the field's north-western boundary via a new 150mm dia. outfall pipe. The new outfall pipe will run alongside the site access track, following the route of the existing outfall pipe currently serving site (see Section 3.4). The existing outfall pipe runs underneath the site access track; as such it will need be removed as part of the access construction works due to its shallow depth.

Water will discharge at a maximum flow rate equivalent to the pre-development greenfield rate 'Qbar'. This restriction in discharge flow rate will be achieved by a new outfall manhole with a flow control unit within, installed immediately downstream of the basin.

Stormwater uphill on the bank adjacent to the east of the site will be intercepted by a second filter drain along the compound's eastern boundary. From this filter drain, water will be conveyed to the new outfall manhole. No change in ground permeability is proposed on the bank; no increase in storm flows is therefore expected so water intercepted by this eastern filter drain can discharge into the north-western ditch without restriction imposed by flow control.

## 5.4 Foul Drainage

There will be no permanent foul drainage from the proposed development.

Any foul drainage from the temporary welfare facilities will be self-contained and disposed off-site appropriately.

### 5.5 Water Quality and Treatment

A Simple Index Approach is adopted as per CIRIA SuDS Manual to determine the suitability of the proposed development's SuDS components in mitigating water quality risks, as per Section 26.7.1 of the SuDS Manual 2015 (CIRIA C753).

- 1. Filtration of water through filter drain along western edge of compound; mitigation indices for filter drain: TSS = 0.4, metals = 0.4, hydrocarbons = 0.4.
- 2. Settlement in attenuation / infiltration basin; mitigation indices for detention basin: TSS = 0.5, metals = 0.5, hydrocarbons = 0.6.
- 3. Filtration of water through vegetation within ditch abutting north-western edge of field: TSS = 0.5, metals = 0.6, hydrocarbons = 0.6.

Table 1 below demonstrates how the pollution hazard index for each contaminant is satisfied by the three stages of water treatment provided as part of the proposed drainage strategy.

Table 1 - Simple Index calculation

Contaminant	Stage 1	Stage 2	Stage 3	Total SUDS	Pollution	Utilisation
Туре				Mitigation	Hazard	
				Index	Index	
TSS	0.4	0.5(0.5)=0.25	0.5(0.5)=0.25	0.90	0.8	1.13
Metals	0.4	0.5(0.5)=0.25	0.5(0.6)=0.3	0.95	0.8	1.19
Hydrocarbons	0.4	0.5(0.6)=0.3	0.5(0.6)=0.3	1.00	0.9	1.11

During the construction phase, temporary silts fences will be installed, providing an additional treatment stage of water filtration.

Refer to Appendix B for indicative drainage details and proposed drainage strategy plan.

## 6 Hydraulic Assessment

A preliminary runoff and attenuation calculation for compound and temporary hardstanding has been undertaken using a HR Wallingford online design tool available from:

#### https://www.uksuds.com/tools/greenfield-runoff-rate-estimation

The inputs taken have been assumed as "worst case" and as such has determined the maximum drainage component extents required for the project. This includes assuming all permanent infrastructure (other than the access track) has an asphalt surface, and that drainage by infiltration is not possible.

A detailed drainage design will be performed following the ground investigation and compound earthing design (to determine surface finishes).

All methods and inputs are taken in accordance with the relevant guidance documents provided in Section 2.

#### 6.1 Greenfield Peak Runoff Rates from Site

Current and future greenfield runoff rates for the development have been estimated using the IH124 Method. Using the mapping software within HR Wallingford Design Tool, the site-specific parameters have been established:

- Standard average annual rainfall between 1941 1970 (SAAR): 979mm.
- Standard percentage run-off: 47%.
- Total drained area: 0.70 ha.
- M5-60 rainfall depth: 14mm.
- Ratio M5-60 / M5-2day: 0.3.

Total drained area is defined as the catchment area for the attenuation basin, which comprises the area inside the compound (0.70 ha). The extents of this area are defined by a hatch labelled 'surface finish typically comprising stone or asphalt' on the Infrastructure Layout in Appendix A.

Refer to Appendix C for the Qbar design tool calculation summary.

The peak runoff rate calculated for a Qbar (1 in 2.3) rainfall event is 5.0 l/s. It is proposed to match this discharge rate through use of a flow control device installed in a manhole positioned immediately downstream of the basin.

### 6.2 Attenuation Storage Required Post Development

The surface water storage volume estimation tool uses a storage assessment method developed by HR Wallingford based on correlations between storage requirements and hydrological characteristics of sites.

Attenuation storage will be provided to accommodate the peak runoff rate calculated up to the critical 1 in 200 storm plus a 40% allowance for climate change. This attenuation requirement was confirmed via email during early liaison with the South Ayrshire Council. A record of this email is included in Appendix E.

As per the calculation described in Section 6.1, allowable discharge from the basin is set to the calculated greenfield runoff rate of  $5.0 \, l/s$ .

The attention volume calculated based on the above criteria is approximately 430m<sup>3</sup>. 3D modelling has been carried out to prove this volume can be accommodated within the site boundary. The attenuation volume should be considered a maximum volume, this assumes that all surface finishes (other than of the access track) are of asphalt and that drainage by infiltration methods is not possible.

Refer to Appendix C for the storage volume calculation and greenfield runoff estimation summary.

## 7 Operation and Maintenance Requirements

All surface water drainage and pollution control features associated with the site will remain private and will be maintained by the site operator.

The following section outlines the proposed maintenance for the various aspects of the drainage system. If necessary, these outline maintenance proposals will be refined when the site is operational to suit specific conditions.

## 7.1 Filter Drain / Discharge Pipe

The anticipated maintenance plan for the filter drains and attenuation basin discharge pipe is outlined in Table 2.

Table 2 - Typical filter drain and discharge pipe operation and maintenance requirements

Filter Drain / Discharge Pipe Maintenance Schedule							
Maintenance Action	Minimum Frequency						
Inspect filter drain / manhole / pipe. Where stone or pipe has become clogged with silt, it will be cleared out	Half yearly						
Remove litter and debris	Half yearly						
Inspect inlets and outlets for blockages, and clear (if required)	Half yearly						

## 7.2 Basin

The anticipated maintenance plan for the basin at the site is outlined in Table 3.

Table 3 - Typical basin operation and maintenance requirements

Basin Maintenance Sche	dule
Maintenance Action	Minimum Frequency
Remove litter and debris	Half yearly
Inspect inlets and outlets for blockages, and clear (if required).	Half yearly
Inspect inlets and outlets for noticeable effects of erosion, suitable erosion protection measures such as reno-mattress or placement of large stones (>150mm) to dissipate water energy levels will be installed at the area affected.	Half yearly
Inspect silt accumulation rates in any forebay and in main body of the pond and establish appropriate removal frequencies	Half yearly
Reseed areas of poor vegetation growth, alter plant types to better suit conditions (if required).	As required, or if bare soil is exposed over 10% or more of the basin treatment area

## 8 Conclusion

A flood risk assessment has been undertaken across the site. The site has been deemed at no specific risk of flooding.

An assessment of the drainage options has also been undertaken, and it has been concluded that drainage by infiltration is unlikely to be a viable option. As such, the current proposal is to drain the site via an attenuation basin, with a restricted discharge rate into the River Ayr.

The required attenuation volume has been calculated as approximately 430m<sup>3</sup>. This should be considered a maximum volume, based on the assumption that all permanent infrastructure (other than the access track) has an asphalt surface and that drainage by infiltration methods is not possible.

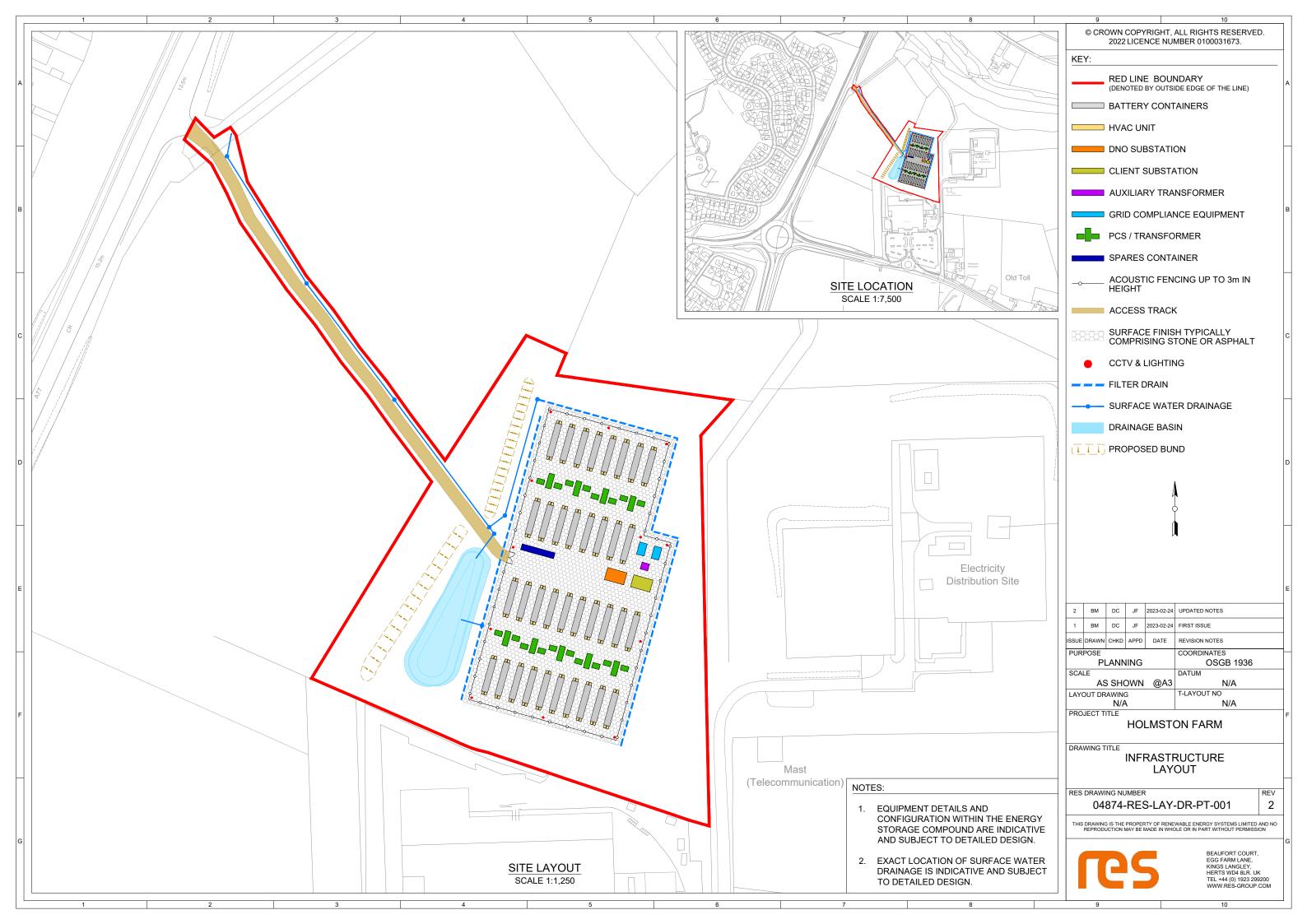
A site investigation, 3D earthworks design, earthing design, and a further assessment of the proposed discharge route will be undertaken to inform the detailed design of the site drainage.

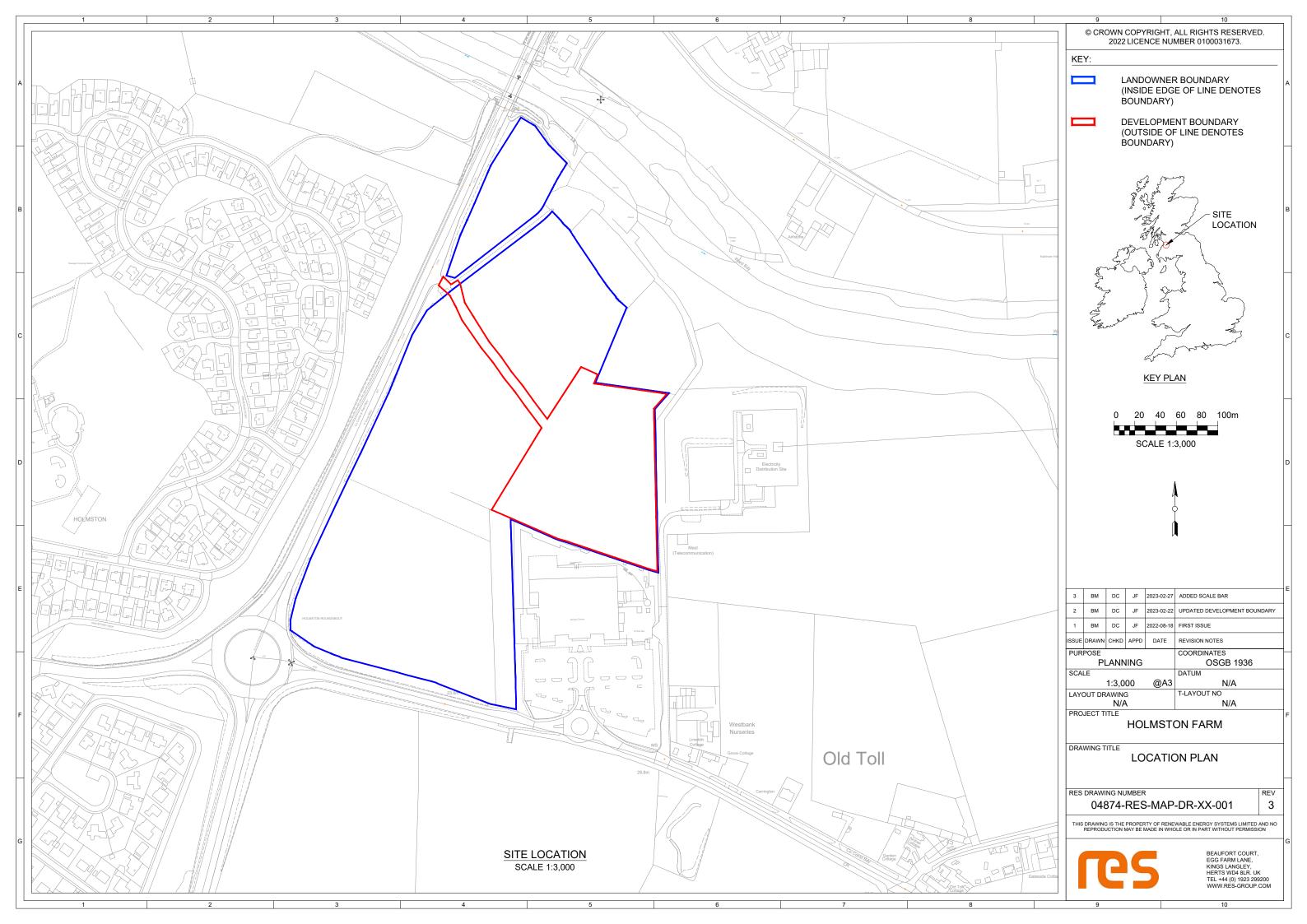
The drainage strategy proposed will provide sufficient water quality treatment as demonstrated using the Simple Index Approach.

## Appendix A Project Drawings

A.1 Infrastructure Layout - 04874-RES-LAY-DR-PT-001

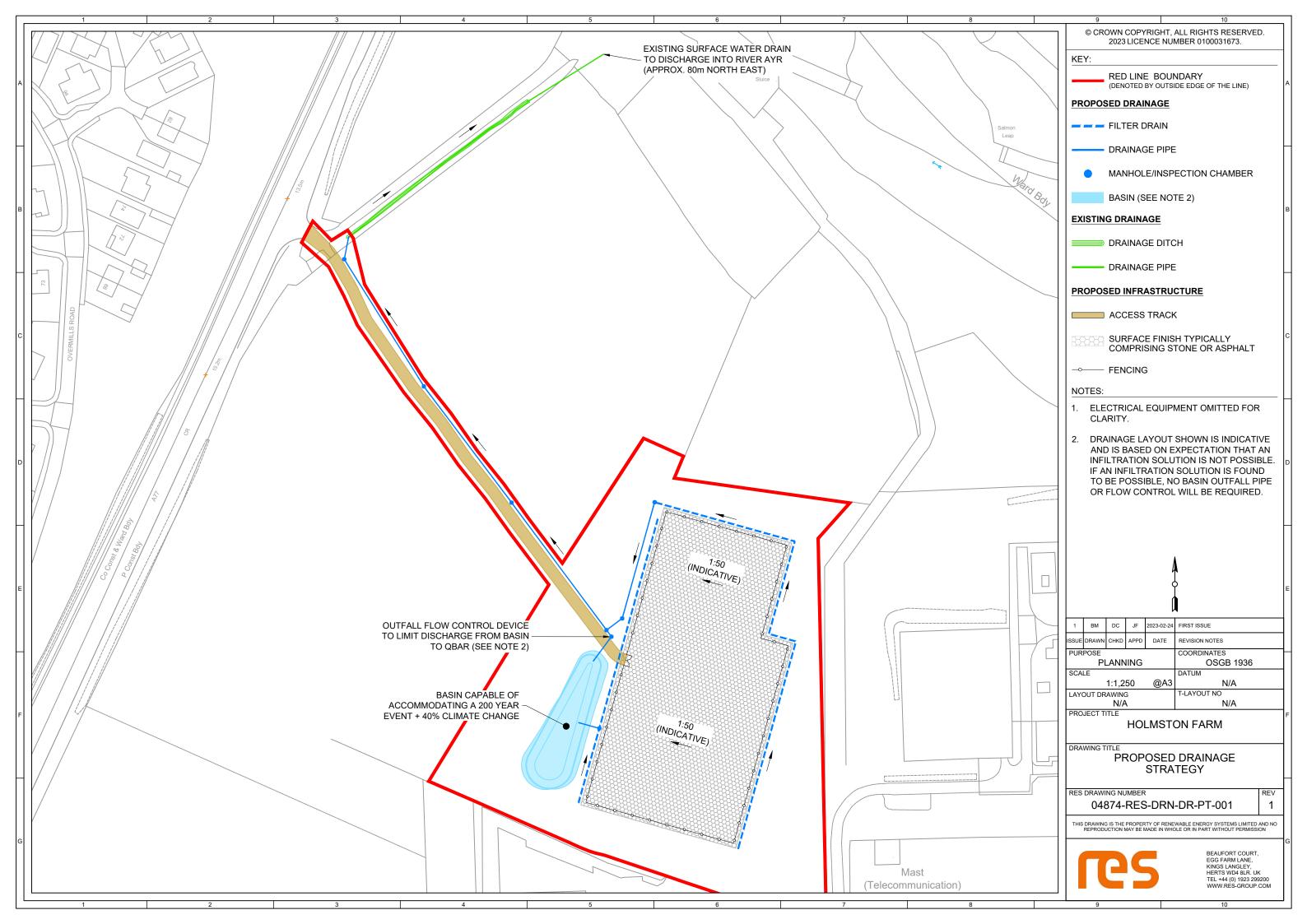
A.2 Location Plan - 04874-RES-MAP-DR-XX-001





## Appendix B Drainage Drawings

- B.1 Proposed Drainage Strategy 04874-RES-DRN-DR-PT-001
- B.2 Typical Drainage Details 04874-RES-DRN-DR-PT-002



## Appendix C Calculations

- C.1 Greenfield Runoff Estimate (HR Wallingford)
- C.2 Storage Volume Calculation

#### Print

## Close Report



# Greenfield runoff rate estimation for sites

www.uksuds.com | Greenfield runoff tool

Calculated by:	Dan C	ole					Site Details		
-	Holmston Farm BESS South Ayrshire					Latitude:	55.45730° N		
Site name:						Longitude:	4.59048° W		
Site location:					Longitude.	4.39040 VV			
This is an estimation of the greenfield runoff rates that are used n line with Environment Agency guidance "Rainfall runoff mana SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the (Defra, 2015). This information on greenfield runoff rates may be the drainage of surface water runoff from sites.				anagement for de d the non-statuto	gement for developments", e non-statutory standards for SuDS		673559337 Nov 28 2022 16:34		
Runoff estimati	Runoff estimation approach IH124								
Site characteris	stics					Notes			
Total site area (ha	otal site area (ha): 0.702				(1) Is Q <sub>BAR</sub> < 2.	0 I/c/ba2			
Methodology					(1) IS QBAR < 2.	0 1/5/11a:			
Q <sub>BAR</sub> estimation r	method: Calculate from SF			m SPR a	and SAAR	When Q <sub>BAB</sub> is < 2.0 l/s/ha then limiting discharge rates are			
SPR estimation m	method: Calculate from SOIL		type	at 2.0 l/s/ha.					
Soil characteris	oil characteristics  Default  Edited				(2) Are flow rates < 5.0 l/s?				
SOIL type:	4								
HOST class:		N/A		N/A		) A //		-01/	
SPR/SPRHOST:		0.47		0.47		Where flow rates are less than 5.0 l/s consent for discharge is usually set at 5.0 l/s if blockage from vegetation and other			
Hydrological ch	naracte	ristics	Def	fault	Edited	· ·		nsent flow rates may be set essed by using appropriate	
SAAR (mm):			979		979	drainage eleme	=	essed by using appropriate	
Hydrological regio	on:		2		2	(2) In CDD/CDD	HOST - 0.22		
Growth curve fac	tor 1 yea	ır:	0.87		0.87	(3) Is SPR/SPR	NOS1 ≤ U.3?		
Growth curve fact	tor 30 ye	ars:	1.95		1.95	Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.		•	
Growth curve fact	tor 100 y	ears:	2.63		2.63			<del>-</del>	
Growth curve factor 200 years:		/ears:	2.99 2		2.99				

Greenfield runoff rates	Default	Edited
Q <sub>BAR</sub> (I/s):	5.02	5.02
1 in 1 year (l/s):	4.37	4.37
1 in 30 years (l/s):	9.79	9.79
1 in 100 year (l/s):	13.2	13.2
1 in 200 years (l/s):	15	15

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.

MS01-004904



#### **Holmston Farm - Storage Volume Calculation**

**Holmston Farm BESS** 

PROJECT NO: 4874

**REFERENCE NO:** 04874-5011522

Issue	Date	Author	Nature and Location of Change
1	14.12.22	Daniel Cole	First issue

Note: revision history should include design stage, revision of load and other relevant information.

#### **Attenuation Storage**

#### 1. INPUT PARAMETERS AND ASSUMPTIONS

#### 1.1 First category of inputs - Hydrological Characteristics

m5-60	14.00	mm F	Five Year - 60 Minute Rainfall Depth (see "Data" Tab)
r	0.30	R	Ratio M5-60/M5-2day (see "Data" Tab)
Location	S/NI	E	E/W (England and Wales) or S/NI (Scotland and Northern Irela
Fc	1.40	<u>C</u>	Climate Change Factor (refer to the hyperlink for what to choos

#### 1.2 Second category of inputs - Catchment Area Characteristics

Ap	0.00	ha	Permeable Area
Ср	0		Permeable area runoff coefficient (see "Data" Tab)
Ai	0.70	ha	Impermeable Area (C= 1 assumed) (ha)
Qa	0.00502	m³/s	Allowable Discharge

#### 2. CALCULATIONS

#### 2.1 First calculation section - effective catchment area calculation

Ae 0	.70	ha	Effective area (	see	"Data"	Tab	J)
------	-----	----	------------------	-----	--------	-----	----

#### 2.2 Second calculation section - calculation to dermine the m5 rainfall for various durations

D (min)	Z1	m5 - D
D (IIIIII)	۷.	(mm)
15.00	0.59	8.26
30.00	0.77	10.78
60.00	1.00	14.00
120.00	1.25	17.50
240.00	1.57	21.98
360.00	1.78	24.92
600.00	2.12	29.68
1440.00	2.84	39.76

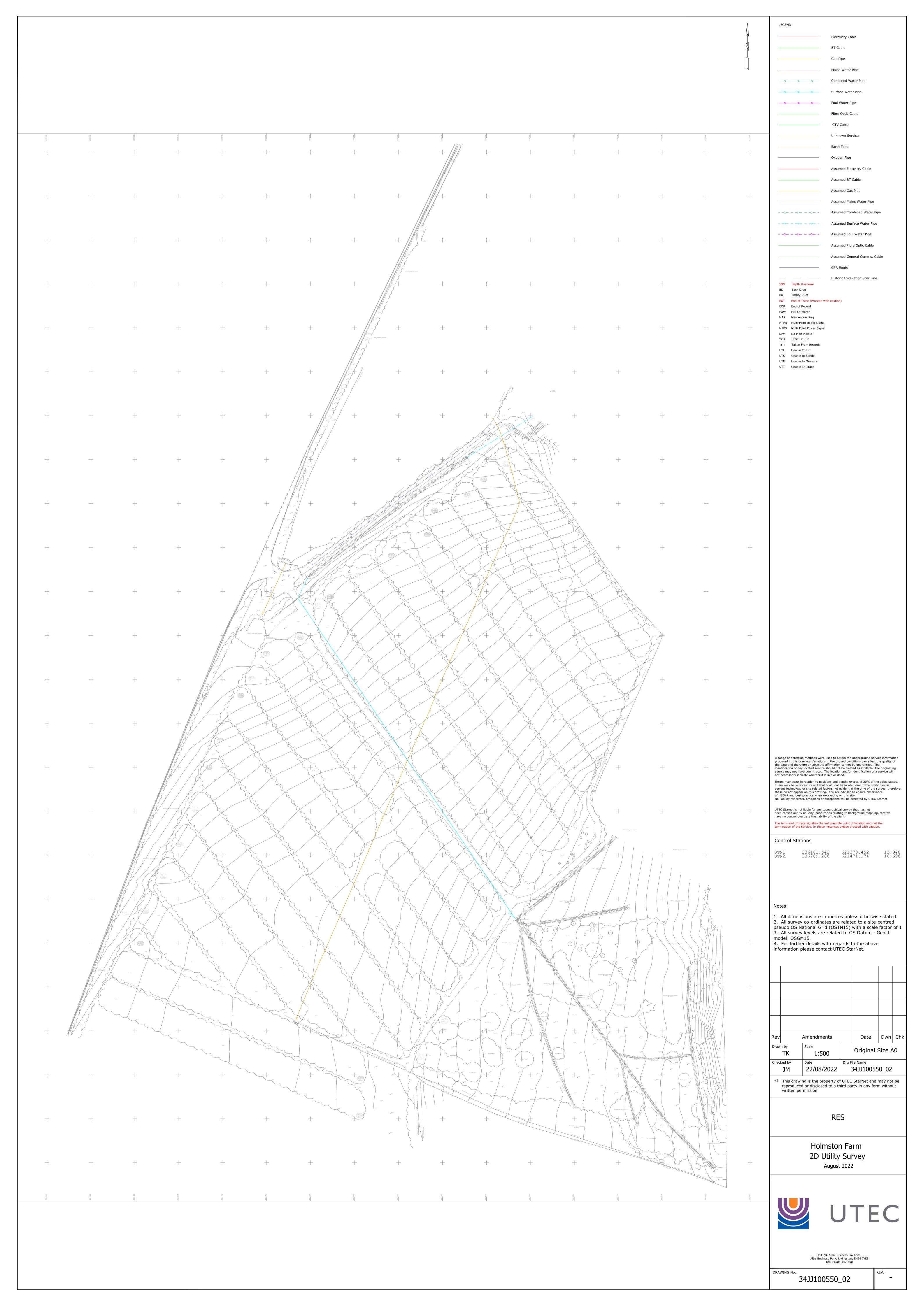
#### 2.3 Third calculation section - attenuation volume calculations for various durations and return periods

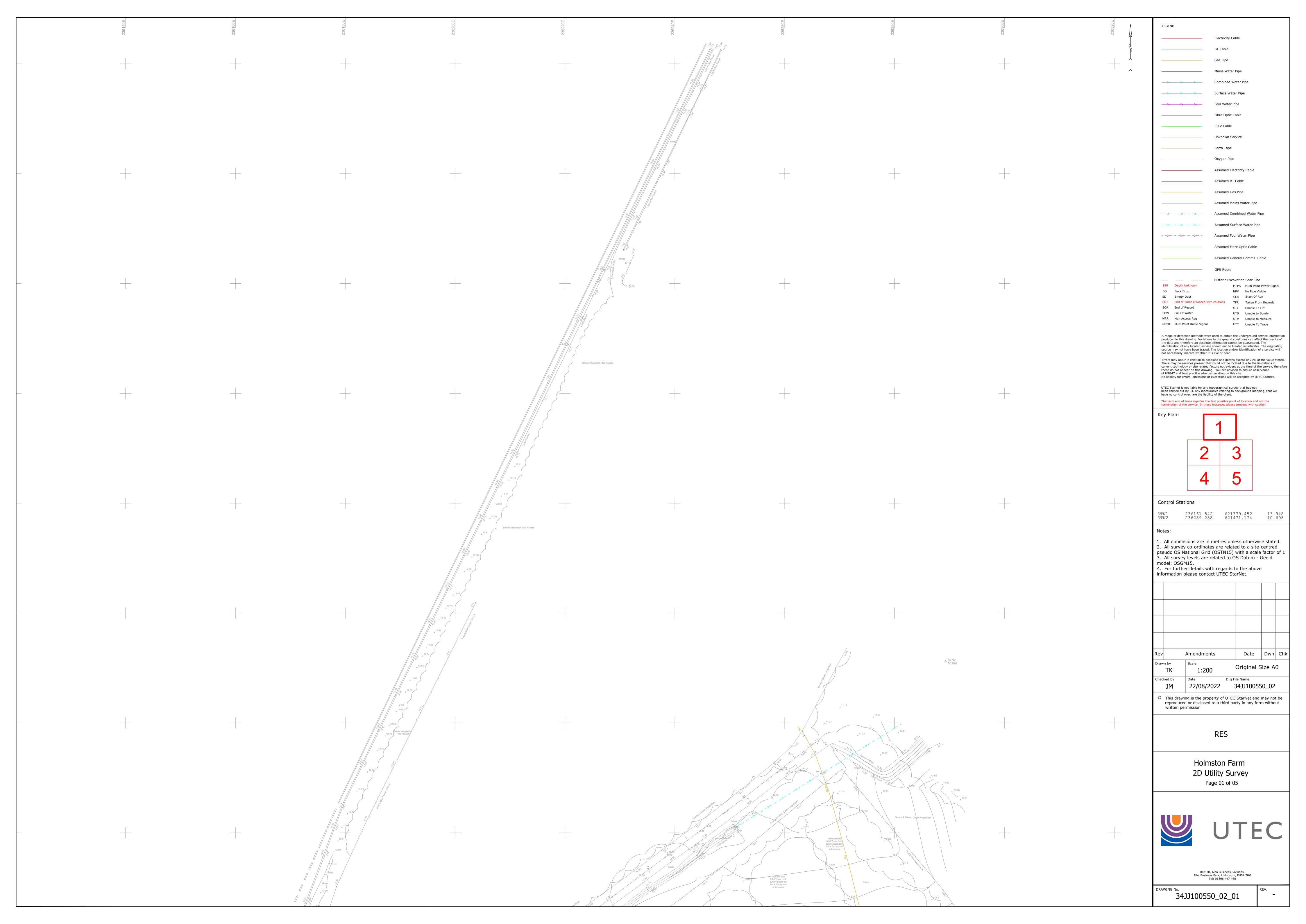
D (min)	Z2	MT-10 (mm)	Inflow Vol m^3	Outflow vol (m^3)	Att Volume	
15.00	0.68	`8´	55	5	50	
30.00	0.68	10	72	9	63	
60.00	0.69	13	95	18	77	
120.00	0.70	17	120	36	83	1 year return period calculation
240.00	0.70	22	152	72	80	
360.00	0.71	25	174	108	65	
600.00	0.72	30	210	181	29	
1440.00	0.74	41	289	434	-145	Note: z2 is calculation in the "Att Da
D (min)	Z2	MT-10 (mm)	Inflow Vol m^3	Outflow vol (m^3)	Att Volume	
D (min)	Z2 1.03					
, ,		(mm)	m^3	(m^3)	Volume	
15.00	1.03	(mm)	m^3 83	(m^3)	Volume 79	
15.00 30.00	1.03 1.03	(mm) 12 16 20 25	m^3 83 109	(m^3) 5 9	Volume 79 100	5 year return period calculation
15.00 30.00 60.00	1.03 1.03 1.02	(mm) 12 16 20	m^3 83 109 141	(m^3) 5 9 18	79 100 123	5 year return period calculation
15.00 30.00 60.00 120.00	1.03 1.03 1.02 1.02	(mm) 12 16 20 25	m^3 83 109 141 175	(m^3) 5 9 18 36	79 100 123 139	5 year return period calculation
15.00 30.00 60.00 120.00 240.00	1.03 1.03 1.02 1.02 1.02	(mm)  12 16 20 25 31	m^3 83 109 141 175 220	(m^3)  5 9 18 36 72	79 100 123 139 148	5 year return period calculation  Note: z2 is calculation in the "Att Da

D (min)	Z2	MT-10 (mm)	Inflow Vol m^3	Outflow vol (m^3)	Att Volume	
15.00	1.18	14	96	5	92	
30.00	1.19	18	126	9	117	
60.00	1.20	23	165	18	147	
120.00	1.20	29	206	36	169	10 year return period calculation
240.00	1.19	36	256	72	184	
360.00	1.18	41	289	108	181	
600.00	1.18	49	344	181	163	National Constant of the WALL Date II Tak
1440.00	1.17	65	457	434	24	Note: z2 is calculation in the "Att Data" Tab
D (min)	Z2	MT-10	Inflow Vol m^3	Outflow vol	Att Volume	
		(mm)		(m^3)		
15.00	1.47	17	120	5	115	
30.00	1.49	22	158	9	149	
60.00	1.49	29	205	18	187	
120.00	1.48	36	255	36	219	30 year return period calculation
240.00	1.47	45	317	72	245	
360.00	1.46	51	358	108	249	
600.00	1.44	60	421	181	241	Note: -0 is solar lation in the "Att Data" Tab
1440.00	1.41	79	553	434	119	Note: z2 is calculation in the "Att Data" Tab
D (min)	Z2	MT-10		Outflow vol	Att	
D (111111)		(mm)	m^3	(m^3)	Volume	
15.00	1.93	22	157	5	152	
30.00	1.97	30	209	9	200	
60.00	1.98	39	272	18	254	
120.00	1.96	48	336	36	300	100 year return period calculation
240.00	1.91	59	413	72	341	
360.00	1.89	66	463	108	355	
600.00	1.85	77	540	181	360	
1440.00	1.77	99	692	434	259	Note: z2 is calculation in the "Att Data" Tab
D (min)	70	MT-10	Inflow Vol	Outflow vol	Att	
D (min)	Z2	(mm)	m^3	(m^3)	Volume	
15.00	2.20	25	178	5	174	
30.00	2.25	25 34	239	9	230	
60.00	2.25	34 44	311	18	293	
120.00	2.23	55	384	36	347	200 year return period calculation
240.00	2.18	67	470	72	398	200 your rotain porrod odiodidatori
360.00	2.14	75	524	108	416	
600.00	2.09	87	611	181	430	
1440.00	1.98	110	775	434	341	Note: z2 is calculation in the "Att Data" Tab
3. RESULTS	1					
Att 1		83	m³			Attenuation volume required in a 1 in 1 year event
Att 5		148	m³			Attenuation volume required in a 1 in 5 year event
Att 10		184	m³			Attenuation volume required in a 1 in 10 year event
Att 30		249	m³			Attenuation volume required in a 1 in 30 year event
Att 100		360	m³			Attenuation volume required in a 1 in 100 year event
Att 200		430	m³			Attenuation volume required in a 1 in 200 year event
, 200		730				. Mondadon volumo roquilod in a 1 in 200 year event

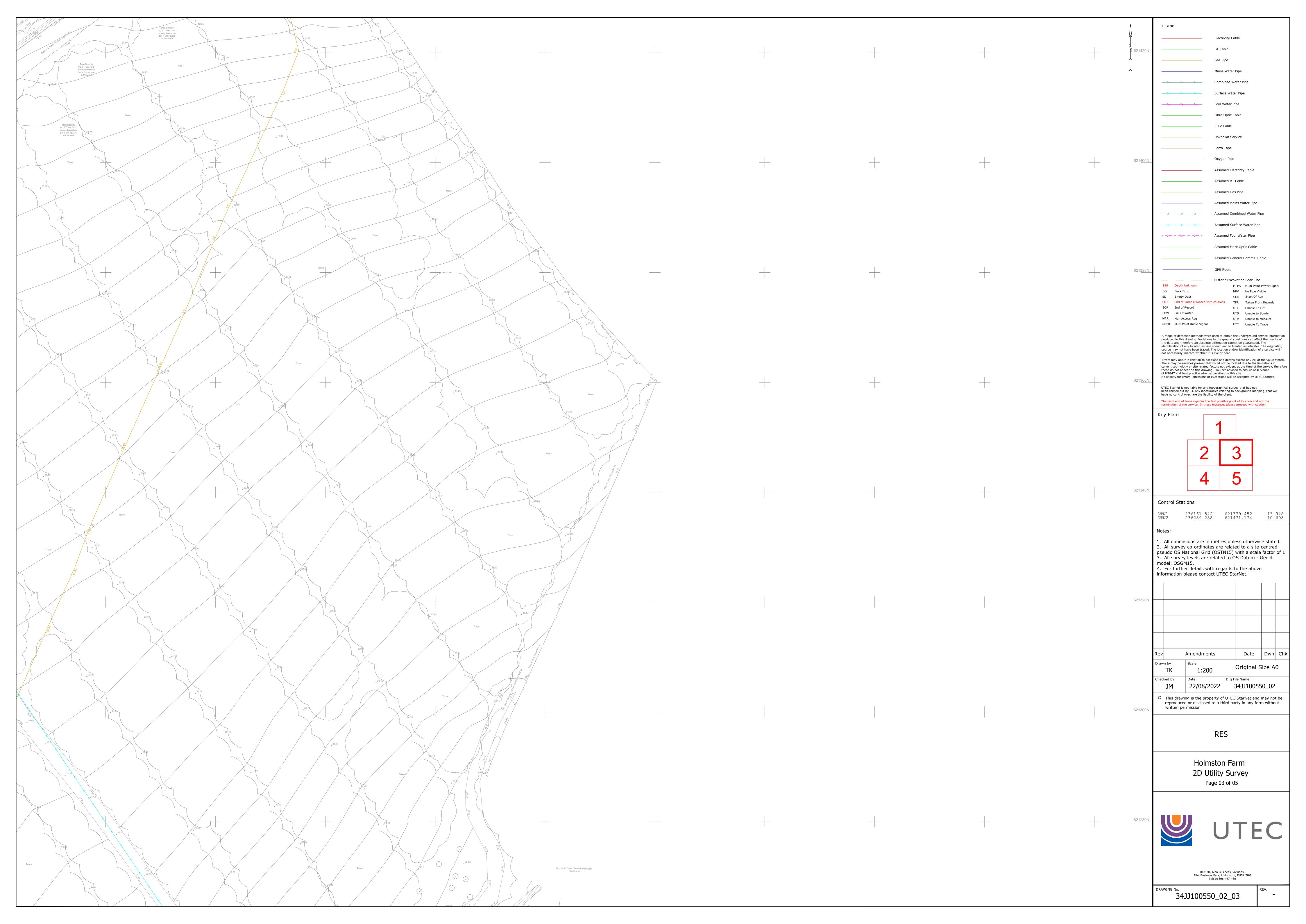
## Appendix D Topographic Surveys

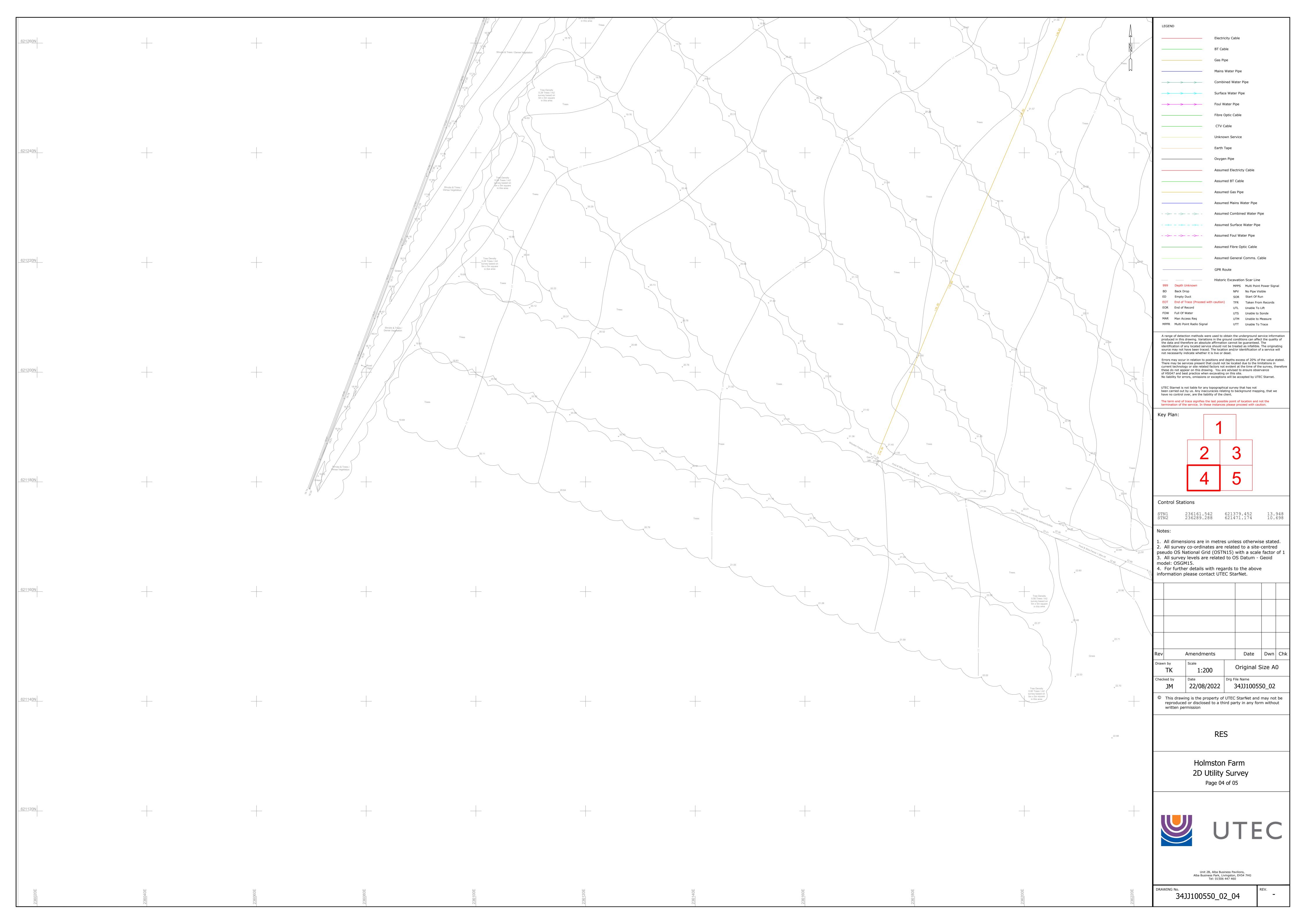
- D.1 Below Ground Survey
- D.2 Topographic Survey

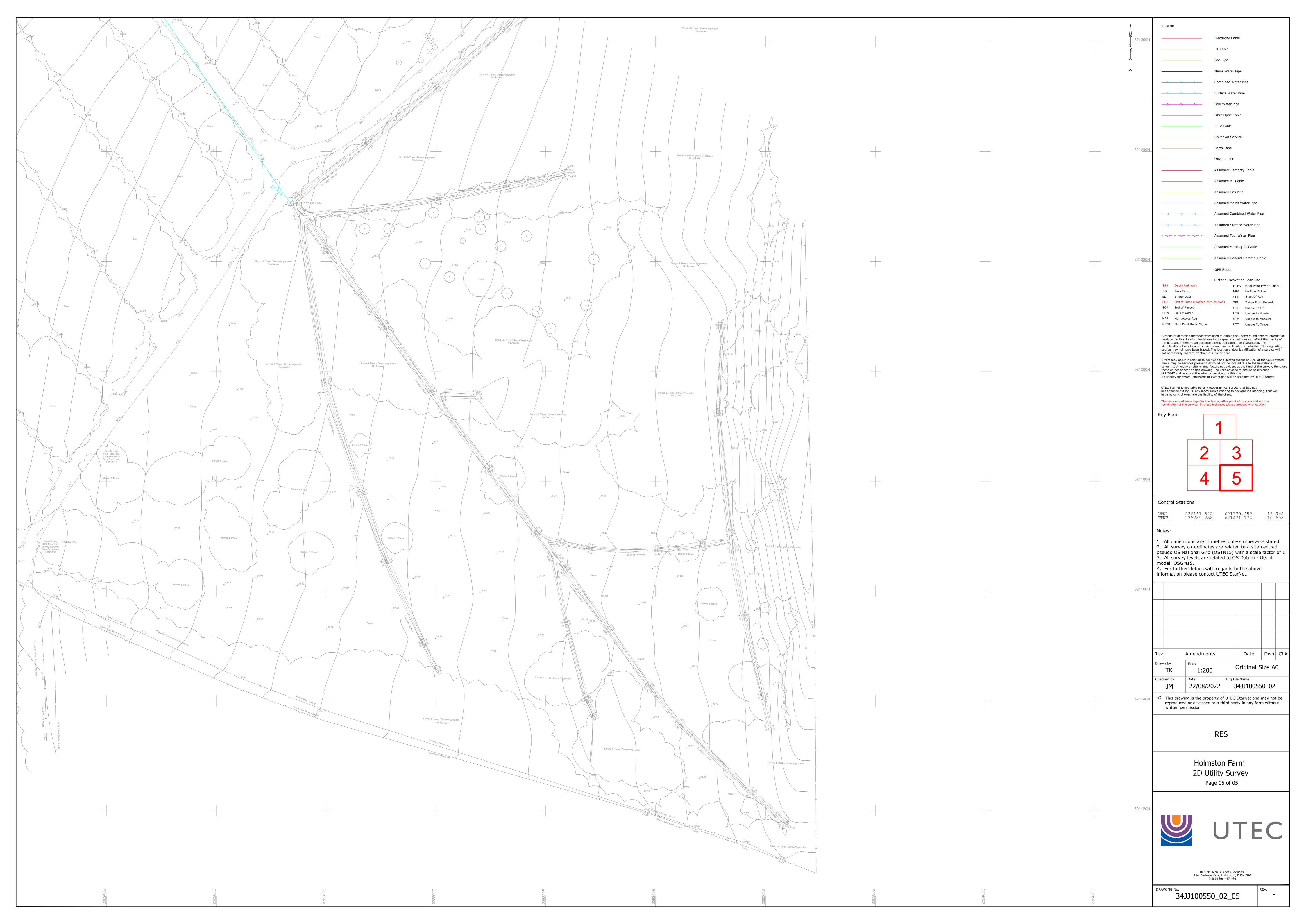


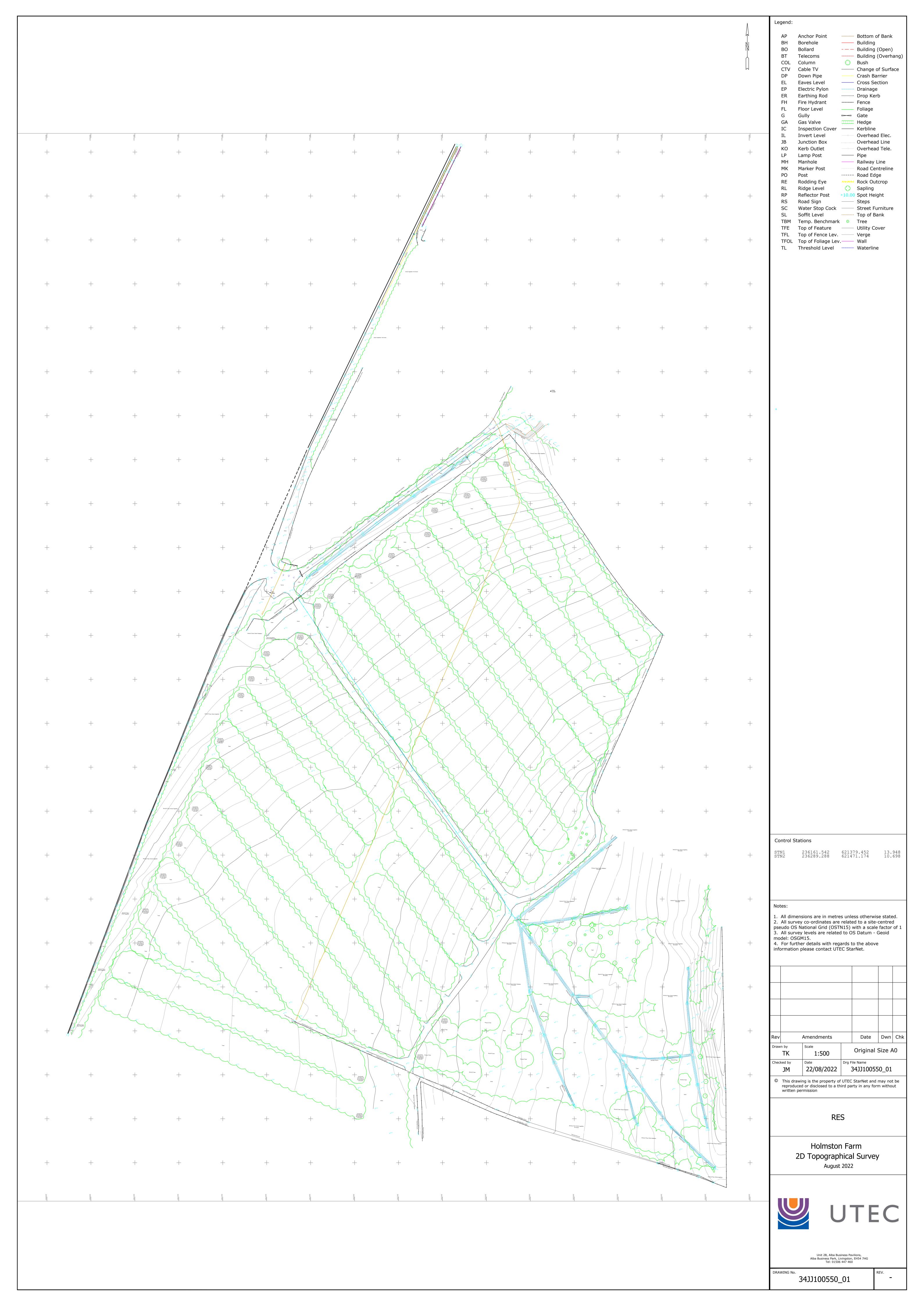


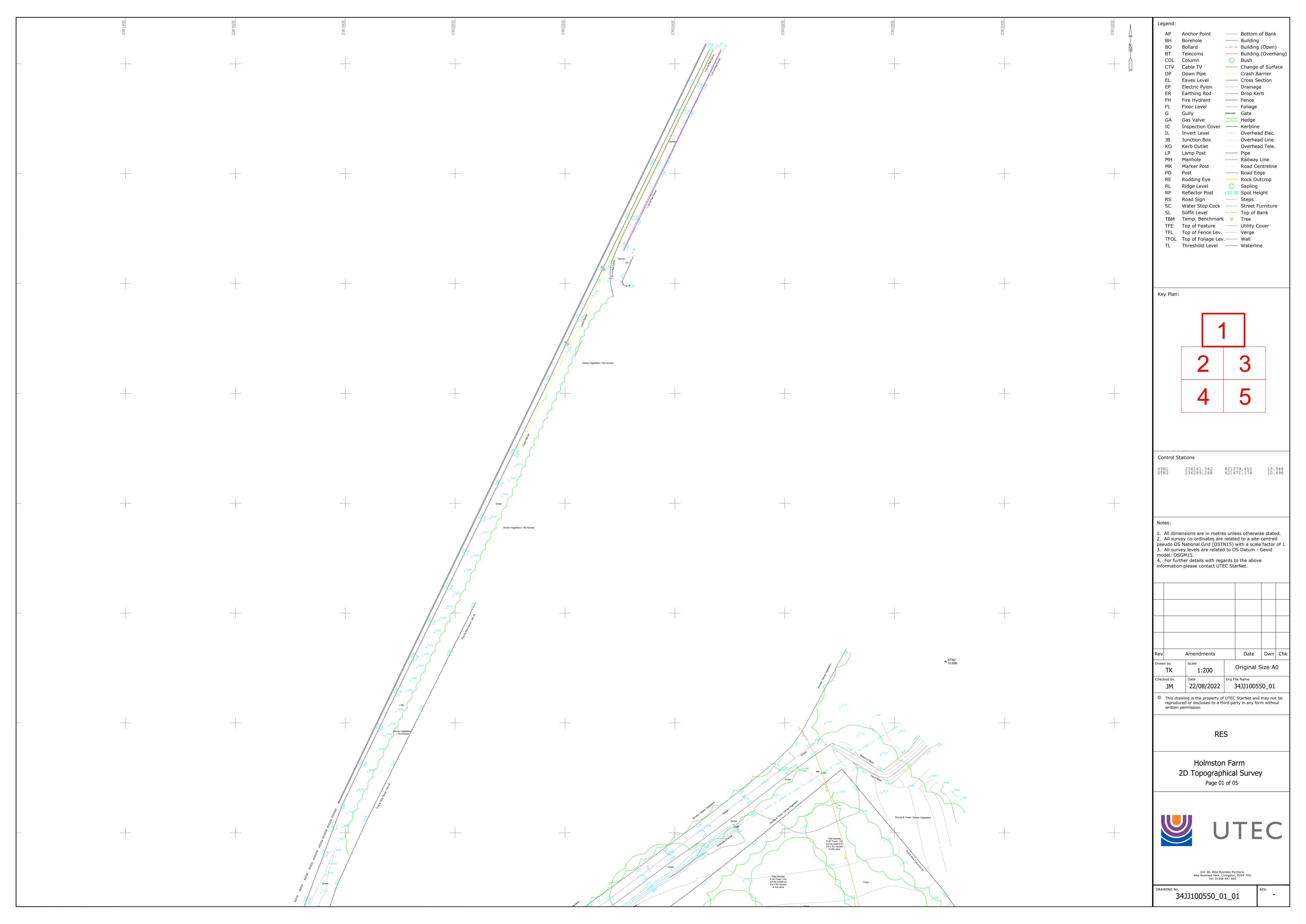


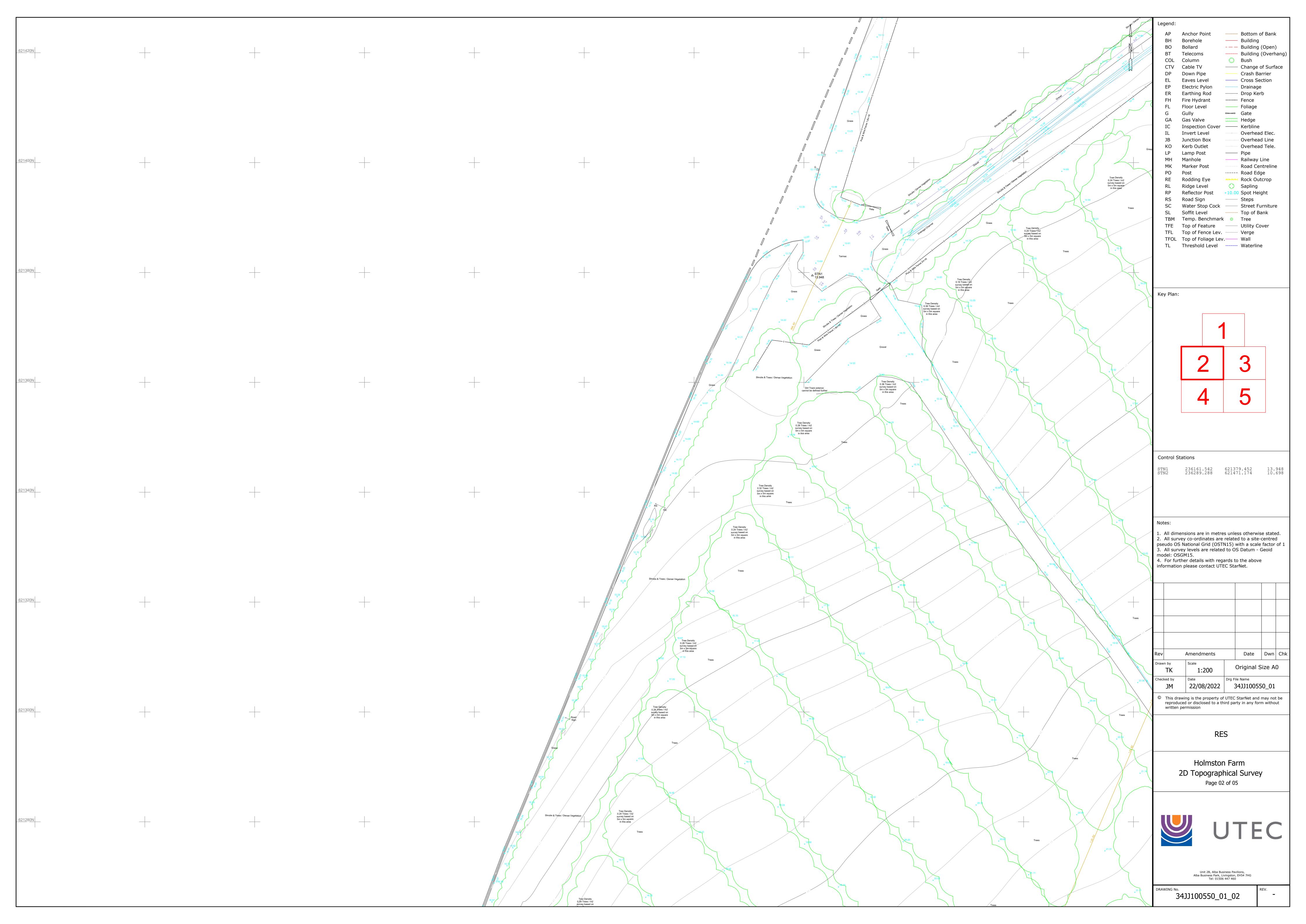


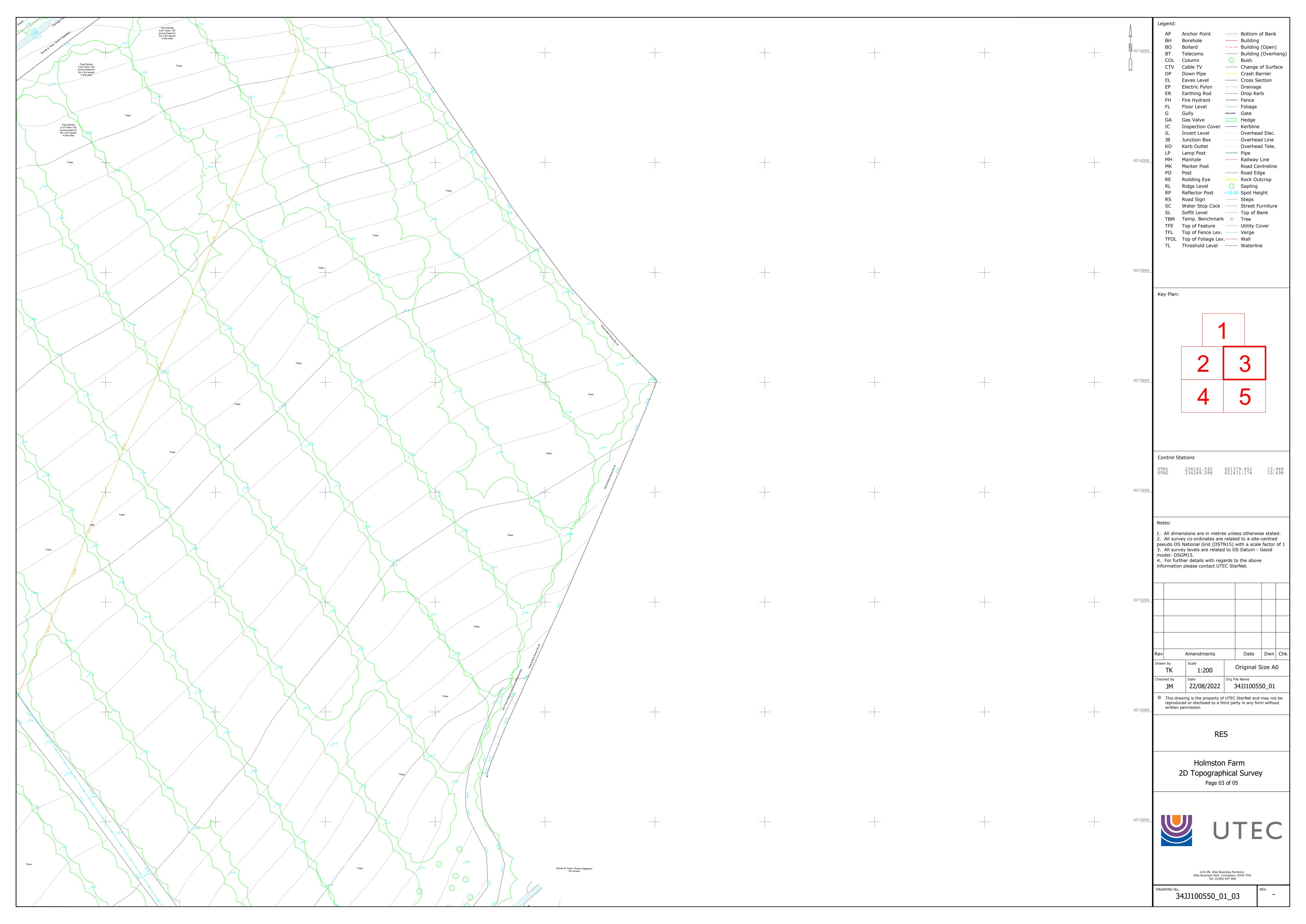


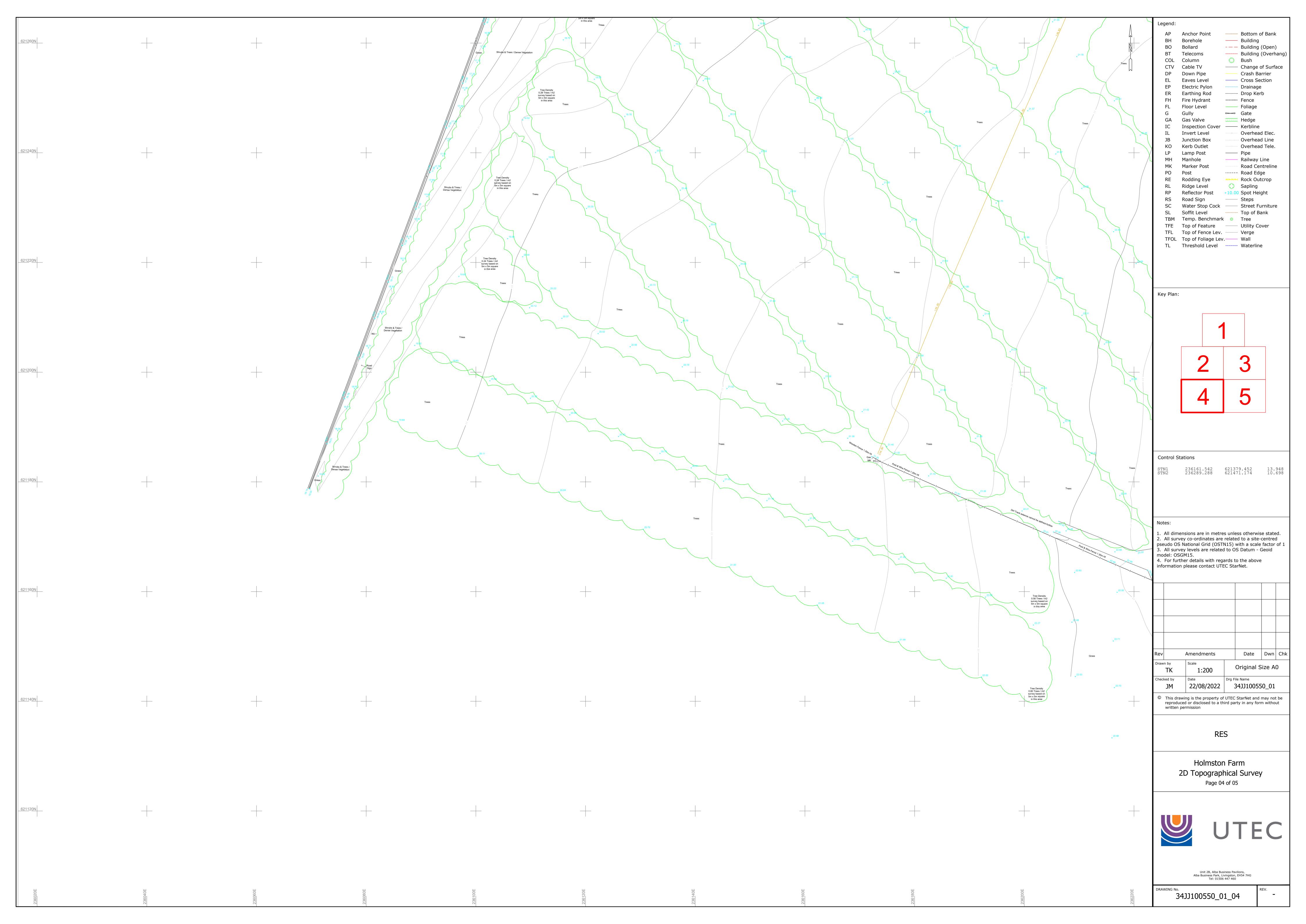


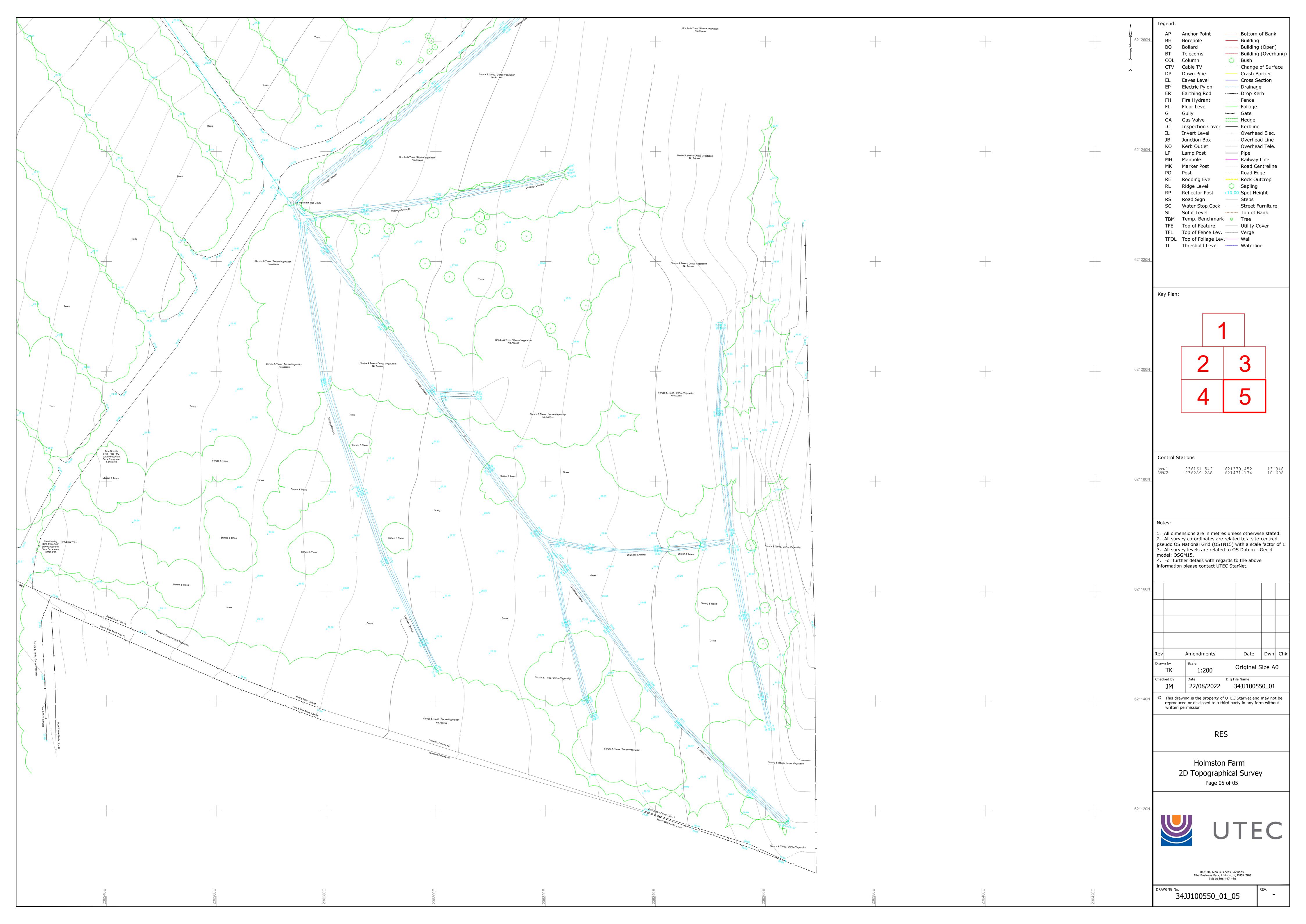












## Appendix E Correspondence

E.1 South Ayrshire Council Drainage Response

#### **Daniel Cole**

From: Greig, Scott <Scott.Greig@ayrshireroadsalliance.org>

**Sent:** 01 November 2022 13:02

To: Daniel Cole

**Subject:** RE: South Ayrshire Council drainage / flood risk criteria for 22/00437/PREAPP - enquiry

[OFFICIAL]

**Follow Up Flag:** Follow up **Flag Status:** Flagged

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**CLASSIFICATION: OFFICIAL** 

#### Afternoon Daniel,

South Ayrshire Council have no specific Guidance Document online for the management of flood risk. However the aim is always to ensure that any proposed development is compliant with the principles of Scottish Planning Policy where you will find useful information.

Please see below comments on your various specific questions.

Scott,

Scott Greig B.Eng., C.Eng., M.I.C.E.
Supervisory Engineer, Bridges - Ayrshire Roads Alliance
Ayr Town Hall
21 Newbridge Street
Ayr
KA7 1JX.

Telephone 01563 576459 07974 443010
Email scott.greig@ayrshireroadsalliance.org
Website www.ayrshireroadsalliance.org

Ayrshire Roads Alliance

A partnership between East Ayrshire Council and South Ayrshire Council





From: Daniel Cole <daniel.cole@res-group.com>

Sent: 27 October 2022 13:48

To: Greig, Scott <Scott.Greig@ayrshireroadsalliance.org>

Subject: South Ayrshire Council drainage / flood risk criteria for 22/00437/PREAPP - enquiry

Good afternoon Scott,

We are currently preparing a planning application for a battery energy storage facility at Holmston Farm, in Ayr – grid ref: N:236312, E:621202, pre-app advice ref: 22/00437/PREAPP.

I'm emailing regarding the criteria we should adhere to in our design / documentation around drainage / flood risk for a planning submission of this nature. I apologise if this information is denoted online, I have searched but have been unable to find it.

The type of criteria I'm seeking clarification on are:

- Criteria for surface water discharge rate limitation Greenfield equivalent rate for the 1 in 200+cc event.
- Critical storm to be attenuated on site

1 in 200 + cc

- Plans / figures to include in documentation

Greenfield equivalent calculations and discharge rates. Outline drainage details including proposed attenuation measures and outfall.

Checks and demonstrations to include in documentation
 Evidence of your internal checking and quality control process.
 Drainage system capacity checks for relevant storm events.
 If public roads then details of the two levels of treatment for road drainage prior to discharge to the water environment.

Any guidance would be appreciated. I would be more than happy to discuss the proposal and any requirements on the phone if you would prefer.

Kind regards,

**Daniel Cole**Civil Design Engineer

daniel.cole@res-group.com | www.res-group.com





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Please consider donating to the Provost's chosen charity for the next two years to help people living with Motor Neurone Disease.

https://eastayrshi.re/provostcharitydonation